ME 50000 – Advanced Thermodynamics Spring 2024

Lecture 26b: Summary of Availability/Exergy

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> Updated material and slides from © Terry R. Meyer

□ Mass balance for CV:

» For CM: m=constant

$$\frac{\mathrm{dm}_{\mathrm{CV}}}{\mathrm{dt}} = \sum_{\mathrm{in}} \dot{\mathrm{m}}_{\mathrm{in}} - \sum_{\mathrm{out}} \dot{\mathrm{m}}_{\mathrm{out}}$$

□ Energy balance for CV:

$$\frac{dE_{CV}}{dt} = \dot{Q} + \dot{W} + \sum_{in} \dot{m}_{in} \left(h + \frac{v^2}{2} + gz \right)_{in} - \sum_{out} \dot{m}_{out} \left(h + \frac{v^2}{2} + gz \right)_{out}$$

» For CM: $dE_{CM} = dU_{CM} + dKE_{CM} + dPE_{CM} = \dot{Q}dt + \dot{W}dt$

□ Entropy Balance for CV:

$$\frac{dS_{CV}}{dt} = \sum_{j} \frac{\dot{Q}_{j}}{T_{b,j}} + \sum_{in} \dot{m}_{in} s_{in} - \sum_{out} \dot{m}_{out} s_{out} + \dot{\sigma}$$
$$\frac{dS_{CM}}{dt} = \sum_{i} \frac{\dot{Q}_{i}}{T_{b,i}} + \dot{\sigma}$$

» For CM:

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□ Availability or non-flow exergy for closed systems:

$$\Phi = m\phi = m[(u - u_0) + P_0(v - v_0) - T_0(s - s_0) + ke + pe]$$

□ Relationship between useful work and availability:

$$\begin{split} W_{\text{act,use,tot}} &= \left(E_2 - E_1\right) + p_o\left(V_2 - V_1\right) - T_o\left(S_2 - S_1\right) - \sum_j Q_j \left(1 - \frac{T_o}{T_j}\right) + T_o \sigma_{\text{tot}} \\ \Rightarrow & W_{\text{act,use,tot}} = \Phi_2 - \Phi_1 - \sum_j Q_j \left(1 - \frac{T_o}{T_j}\right) + T_o \sigma_{\text{tot}} \\ \text{or} & W_{\text{act,use,CM}} = \Phi_2 - \Phi_1 - \sum_i Q_i \left(1 - \frac{T_o}{T_i}\right) + T_o \sigma_{\text{CM}} \\ \end{split}$$

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□ Stream availability or flow exergy:

$$\dot{\Psi} = \dot{m}\psi = \dot{m}\left[(h - h_o) + \frac{v^2}{2} + g(z - z_o) - T_o(s - s_o)\right]$$

□ Exergy balance for CV:

$$\frac{\mathrm{d}\Phi_{CV}}{\mathrm{d}t} = \sum_{in} \dot{m}_{in} \psi_{in} - \sum_{out} \dot{m}_{out} \psi_{out} + \sum_{j} \dot{Q}_{j} \left(1 - \frac{T_{o}}{T_{j}} \right) + \left(\dot{W}_{CV} + p_{o} \frac{\mathrm{d}V_{CV}}{\mathrm{d}t} \right) - T_{o} \dot{\sigma}_{CV}$$
$$\dot{W}_{CV} = \dot{W}_{use} - p_{o} \frac{\mathrm{d}V_{CV}}{\mathrm{d}t}$$

□ Irreversibilities or exergy destruction

$$\dot{I}_{CV} = T_o \dot{\sigma}_{CV}$$

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□ Heat Engine (power cycle):

» Thermal efficiency (based on First Law):

$$\eta_{\text{thermal,HE}} = \frac{|W_{net}|}{Q_H} = \frac{|Q_H| - |Q_L|}{|Q_H|} = 1 - \frac{|Q_L|}{Q_H}$$

» Reversible heat engine (Carnot heat engine)

$$\eta_{\text{thermal,HE,rev}} = \eta_{\text{Carnot,HE}} = 1 - \frac{|Q_L|}{|Q_H|} = 1 - \frac{T_L |\Delta S_L|}{T_H |\Delta S_H|} = 1 - \frac{T_L}{T_H}$$

» Second Law efficiency/effectiveness

- For reservoirs:

$$\varepsilon_{II,HE} = \eta_{II,HE} = \frac{\eta_{thermal,HE}}{\eta_{Carnot,HE}} = \frac{|\dot{W}_{out,use}|}{\dot{\Phi}_{Q_H}} = \frac{\eta_{th,act}|\dot{Q}_H|}{|\dot{Q}_H|\underbrace{\left(1 - \frac{T_0}{T_H}\right)}_{=\eta_{th,Carnot}}}$$
- Finite temperatures:

$$\varepsilon_{II,HE} = \eta_{II,HE} = \frac{|\dot{W}_{out,use}|}{\Delta \dot{\Psi}_H}$$

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□ Heat Pump (Air-conditioning/Refrigeration):

» Coefficient of Performance (cooling mode C):

$$COP_{C,act} = \frac{|\dot{Q}_L|}{\dot{W}}$$

» Reversible heat pump cycle (cooling mode)

$$COP_{C,Carnot} = \frac{T_L}{T_H - T_L}$$

- » Second Law efficiency/effectiveness
 - For reservoirs:

$$\varepsilon_{HP,C} = \frac{COP_{C,act}}{COP_{C,Carnot}} = \frac{\dot{\Phi}_{Q_L}}{\dot{W}}$$

- General expression:

$$\varepsilon_{\rm HP,C} = \frac{COP_{C,act}}{COP_{C,Carnot}}$$

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□ Heat Pump (Heating):

» Coefficient of Performance (heating mode H):

$$COP_{H,act} = \frac{\left|\dot{Q}_{H}\right|}{\dot{W}}$$

» Reversible heat pump cycle (heating mode)

$$COP_{H,Carnot} = \frac{T_H}{T_H - T_L}$$

- » Second Law efficiency/effectiveness
 - For reservoirs:

$$\varepsilon_{HP,H} = \frac{COP_{H,act}}{COP_{H,Carnot}} = \frac{\dot{\Phi}_{Q_H}}{\dot{W}}$$

- General expression:

$$\varepsilon_{\rm HP,H} = \frac{COP_{H,act}}{COP_{H,Carnot}}$$

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- □ Turbine (adiabatic):
 - » Isentropic efficiency:

$$\eta_{\rm t,is} = \frac{|w_{\rm actual}|}{|w_{\rm isentropic}|}$$

» Exergetic efficiency/effectiveness

$$\varepsilon_t = \frac{\left|\dot{W}_{\rm actual}\right|/\dot{m}}{\psi_{in} - \psi_{out}}$$

□ Compressor/Pump (adiabatic):

» Isentropic efficiency:

$$\eta_{\rm c,is} = \frac{w_{\rm isentropic}}{w_{\rm actual}}$$

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» Exergetic efficiency/effectiveness:

$$\varepsilon_t = \frac{\psi_{out} - \psi_{in}}{\dot{W}_{actual}/\dot{m}}$$

□ Heat exchanger without mixing and adiabatic (c=cold stream; h=hot stream):

» Exergetic efficiency/effectiveness

$$\varepsilon_{HX} = \frac{\dot{m}_{c}(\psi_{c,out} - \psi_{c,in})}{\dot{m}_{h}(\psi_{h,in} - \psi_{h,out})}$$

□ Direct contact heat exchanger (mixing) adiabatic:

» Hot stream: 1

» Cold stream: 2
$$\varepsilon_{mix} = \frac{\dot{m}_2(\psi_3 - \psi_2)}{\dot{m}_1(\psi_1 - \psi_3)}$$

» Mixed stream: 3

□ General definition of second law efficiency/effectiveness:

$$\varepsilon_{II} = \frac{\text{Exergy recovered}}{\text{Exergy supplied}} = 1 - \frac{\text{Exergy destroyed}}{\text{Exergy supplied}}$$

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